Exercise 3L2. Deterministic landslide hazard assessment

Some background information:

The final aim of large scale landslide hazard analysis (scales larger than 1:10,000) is to create quantitative hazard maps. The hazard degree can be expressed by the *Safety Factor*, which is the ratio between the forces that make the slope fail and those that prevent the slope from failing. Fvalues larger than 1 indicate stable conditions, and F-values smaller than 1 unstable. At $F=1$ the slope is at the point of failure.

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The infinite slope model can be used on profiles as well as on pixels. The entire analysis requires first the preparation of the data base. The parts on groundwater modelling and the modelling of seismic acceleration are not shown here. For more information see Van Westen (1993). In this exercise only the calculation of average safety factors will be done for different scenarios. These average safety factor maps could be used in the creation of failure probability maps.

Visualization of the input data

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In this exercise the slope stability analysis is made by using only two parameter maps: **Soildepth** (thickness of soil) and **Slope_map** (slope angles in degrees).

• Open the maps **Soildepth** and **Slope_map** and check the values in the maps. Click OK in the Display Options dialog box. The map is displayed.

We assume that:

 M: $Zw/Z =$

the depth of the possible failure plane is taken at the contact of the soil and the underlying weathered rock material.

All soils have the same values for Cohesion, friction angle and unit weight.

In the first part of the exercise we will calculate the stability of the soil cover using only one single value of cohesion, friction angle and bulk density. The consequence of this is that safety factors will not be calculated for the entire area, but only for the areas where there is soil overlying the bed rock.

Besides soil depth which is assumed to be the same as the depth to the failure surface, and the slope of the terrain, we also need to know the other parameters of the infinite slope formula. From laboratory analysis the following average values are known:

Slope_map

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 $tan(\phi')$ = tangent of the effective angle of shearing resistance = 0.625

= effective angle of shearing resistance $(°)$ = 32 °

The only unknown parameter yet is the depth of the water table. In the formula this is expressed as the value m, which is the relation between the depth of the water table and the depth of the failure surface.

Sine and Cosine

The ILWIS functions for sine and cosine only work with input values in radians, while our map Slope_map is in degrees. Therefore we need to convert to slope map from degrees to radians first.

Preparation of the data

Before you can start with the analysis, you need to reorganize the map **Slope_map**. In the calculation we need three parameters that are derived from the slope:

 $sin(slope) =$ the sine of the slope

 $cos(slope) =$ the cosine of the slope

 $cos2(slope) = cos(slope)*cos(slope)$

The ILWIS functions for sine and cosine only work with input values in radians, while our map Slope is in degrees. Therefore we need to convert to slope map from degrees to radians first. ILWIS has the function Degrad for that:

Degrad(Slope) degrees to radians function: slope*2π/360

• Type the following formula on the command line:

Slrad:=degrad(Slope_map)↵

Accept the default minimum, maximum and precision.

• Open the result map and compare the values of the map **Slrad** with those of the map **Slope_map**. With the pixel information click in some points of the map and read the values in degree and in radians. For example: you can type in the command line of ILWIS the following formula:

?10.77*2*3.14/360

Now you have the slope in radians, and you can calculate the sine and cosine. You will calculate individual maps for these so that the Safety factor formula (formula 6.1) can be calculated easier.

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Now all necessary parameters for the formula are known, except for the parameter *m* related to the groundwater depth.

Creating a function for the infinite slope formula

In this dialog box you can edit the expression of the function. Now the expression is:

Function fs(Value Cohesion,Value Gamma,Value M,Value Gammaw,Value Z,Value Co2,Value Tanphi,Value Si,Value Co) : Value Begin Return (Cohesion +(Gamma-M*Gammaw)*Z*Co2*Tanphi) /(Gamma*Z*Si*Co)

End;

As you can see the function contains the following variables (listed in the first line):

- Value Cohesion: the value for the effective cohesion.
- Value gamma: the value for the unit weight of soil.
- Value m: the value for the relation z_w/w .
- Value gammaw: the value for the unit weight of water.
- Value z: the value for the depth of failure surface below the surface.
- Value co2: the value for the square of the cosine of the slope.
- Value tanphi: the value for the tangent of the effective angle of shearing resistance.
- Value si: the value for the sine of the slope.
- Value co: the value for the cosine of the slope.

However, a number of these variables are fixed. You will use them for all calculations: The fixed variables are: Value Cohesion (10000 Pa), Value Gammaw (10000 N/m3), Value Z (raster map **Soildepth**), Value Co2 (raster map **Co2**), Value Tanphi (**0.625**), Value Si (raster map **Si**), and Value Co (raster map **Co**).

So you can simplify the function considerably, so that it looks like:

```
Function fs(Value Gamma,Value M) : Value 
Begin 
Return(10000+((Gamma-m*10000)*Soildepth*Co2*0.625)) 
/(Gamma* Soildepth *Si*Co) 
End;
```
As you can see there are only two variables: Value Gamma and Value M.

Calculating Safety Factors for groundwater scenarios

Now that the function is created, you can start to calculate safety factor maps for different scenarios. In the first part you will calculate the safety factors for different scenarios where only rainfall is the triggering factor. You will not yet look at the influence of an earthquake.

Dry condition

You will first calculate the safety factor for the soils under the assumption that the soil is completely dry. In that case the parameter m is equal to zero.

Now you can start with the actual calculation of the average safety factor map representing the situation under dry conditions. The two variables for the function *fs* are **11000 (Value Gamma)** and **0 (Value M)**.

The resultant map (**Fdry**) will have some pixels with missing values indicated by a question mark (?). You can investigate these pixels and see that the values of the pixels cannot be calculated either because they lack soil or because they are flat areas. Both conditions indicate stability and thus can be safely grouped as stable.

As you can imagine a situation with a completely dry situation does not occur in a tropical region such as RiskCity, which receives quite a lot of rainfall each year. In any case the map **Fdry** gives the most stable situation. Let us see how much percent of the area is unstable under these conditions. In order to know that we will first classify the map **Fdry** into three classes:

Unstable $=$ safety factor lower than 1

Critical = safety factor between 1 and 1.5

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100 Stable

- Use the Slicing operation to classify the map **Fdry** with the domain **Stabil** into the map **Fdryc**.
- Calculate a histogram of the map **Fdryc** and write down the percentages of the three classes in a table on a sheet of paper with the column name **Dry**. Later we will calculate the values for other situations.

The percentage of the pixels classified as unstable gives you an indication of the error, since the occurrence of unstable pixels under fully dry conditions is not possible.

Completely saturated condition

The next scenario that you will evaluate is a condition in which the slopes are completely saturated. This is also not a very realistic situation, but it will give us the most pessimistic estimation of slope stability, with only one triggering factor involved (rainfall leading to high perched watertables).

When we have a saturated soil, the *m* factor from the infinite slope formula is equal to 1. This means that the watertable is at the surface. There is also another parameter that will vary when the soil is completely saturated, which is $γ$:

The two variables for the function *fs* are **16000 (value gamma)** and **1 (value m).**

Now that we have calculated all scenarios, we can compare them. This can be done in a table.

• Draw conclusions on the effect of the groundwater on the stability of the soils in the area.

Partially saturated condition

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- Now design some scenarios yourself where you use M values that vary between 0 and 1, and see the effect on the stability.
- Draw conclusions on the effect of the groundwater on the stability of the soils in the area.

For experienced ILWIS users

) **For experienced ILWIS users:**

Using different values for cohesion and friction angle

It is also important to include different values for cohesion, friction angle and unit weight of soils for different soil or lithological types. You can do that by adding columns **Cohesion, FrictionAngle** and **Gamma** to the table **Lithology**.

) **For experienced ILWIS users:**

Include earthquake acceleration

Iit is also possible to include earthquake acceleration in the equation for the factor of safety. You could try to make a function for that based on the formula given below, and test this out for a few scenarios of earthquake acceleration and M values.

 $F = \frac{c' + z(\gamma \cos^2 \beta - \rho a_h N \cos \beta \sin \beta - \gamma_w m \cos^2 \beta) \tan \varphi'}{z(\gamma \sin \beta \cos \beta + \rho a_h N \cos^2 \beta)}$

- **C' = effective cohesion (Pa)**
- **z = depth of failure surface below terrain surface**
- **γ = unit weight of soil (Nm-3)**
- **β = terrain suface inclination (degrees)**
- **ρ = bulk density (kgm-3)**
- **Ah = peak horizontal acceleration in rock (ms-2)**
- **N = amplification of seismic acceleration in soil**
- γ_w = unit weight of water (Nm⁻³)
- **M** = groundwater/soil thickness ration z_w/z
- Z_w = height of the water table above failure surface (m)
- **φ' = effective angle of shearing resistance (degrees)**